# NANYANG TECHNOLOGICAL UNIVERSITY SCHOOL OF CIVIL AND STRUCTURAL ENGINEERING 

## CV272- NUMERICAL METHODS

## Tutorial 2: Interpolation II (Evenly and unevenly-spaced data)

1. Given that $x_{0}, \ldots x_{3}$ are equally-spaced at intervals $h$, show that Lagrange's interpolation formula with $n=3$ may be written as

$$
\begin{gathered}
f(x)=-\frac{(s-1)(s-2)(s-3)}{3!} f_{o}+\frac{s(s-2)(s-3)}{2} f_{1}-\frac{s(s-1)(s-3)}{2} f_{2} \\
+\frac{s(s-1)(s-2)}{3!} f_{3}
\end{gathered}
$$

where $\quad s=\frac{\left(x-x_{o}\right)}{h}$
2. The bending moments $(M)$ at various points $x$ meters from one end of a beam were recorded in Table Q2.

Table Q2

| $x(\mathrm{~m})$ | 1.0 | 2.0 | 4.0 | 7.0 |
| :--- | ---: | ---: | ---: | ---: |
| $M(\mathrm{kNm})$ | 109.4 | 195.0 | 280.0 | 135.60 |

Estimate the bending moment at $x=2.8 \mathrm{~m}$ (up to 3 decimal places) from
(a) Newton's divided-difference interpolation formula of degree 3. (Ans. 243.873)
(b) Lagrange's interpolation formula, using only the first 3 data points. (Ans. 242.792)

Without recalculating, compute the error in your result for part (b) for ignoring the $4^{\text {th }}$ data print. (Ans. 1.081)
3. The vertical stress $\sigma_{z}$ under the corner of a rectangular area subjected to a uniform load of intensity $q$ is given by the solution of Boussinesq's equation:

$$
\sigma_{z}=q f_{z}(m, n)
$$

where $q$ is equal to the load per unit area and
$f_{Z}$ is called the influence value and $m$ and $n$ are
dimensionless ratios with $m=a / z$ and $n=b / z$
where $a, b$ and $z$ are dimensions defined in
Figure Q3.
The values of $f_{z}$ at various $m$ and $n$ are given in Table Q3.
If $\mathrm{a}=5.6 \mathrm{~m}, \mathrm{~b}=13 \mathrm{~m}$, compute $\mathrm{r}_{\mathrm{Z}}$ at a depth 10 m below the corner of a rectangular footing that is subjected to a total load of 100 tons, employing a quadratic formula in $n$ and m. (Ans. 0.13897)

Table Q3 - Influence Value $f_{z}$
m $\quad n=1.2 \quad n=1.4 \quad n=1.6$
$\begin{array}{lllll}0.1 & 0.02926 & 0.03007 & 0.03058\end{array}$
$\begin{array}{lllll}0.2 & 0.05733 & 0.05894 & 0.05994\end{array}$
$\begin{array}{lllll}0.3 & 0.08323 & 0.08561 & 0.08709\end{array}$
$\begin{array}{llll}0.4 & 0.10631 & 0.10941 & 0.11135\end{array}$
$0.50 .12626 \quad 0.130030 .13241$
0.60 .143090 .147490 .15027
$\begin{array}{lllll}0.7 & 0.15703 & 0.16199 & 0.16515\end{array}$
$\begin{array}{lllll}0.8 & 0.16843 & 0.17389 & 0.17739\end{array}$


Figure Q3
4.. Table Q4 shows the experimental results of deflections, $d$, of a 6 meter uniform beam subjected to a non-uniformly distributed load. Due to a faulty dial gauge, the deflection record at point 5 is invalid. Note that $x$ is the distance from one end of the beam.

## Table 04

| Point | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $x(\mathrm{~m})$ | 0.75 | 1.50 | 2.25 | 3.00 | 3.75 | 4.50 | 5.25 |
| $d(\mathrm{~mm})$ | 4.5 | 18.0 | 30.0 | 45.0 | $?$ | 15.0 | 6.0 |

(a) Using a $4^{\text {th }}$ degree polynomial, determine the deflection at point 5 .
(Ans. 38.701)
(b) Strengthening is required for the part of the beam where the deflections exceed 30 mm . Using a 3rd degree polynomial, determine the length of the beam where strengthening is required. For point 5 , use the computed deflection in part (a). (Ans. Length $=4.086-2.25 \mathrm{~m}$ )
TKH/jam
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